

Control Systems II

System Modelling

$$A = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix}, B = \begin{bmatrix} \frac{\partial f_1}{\partial u} \\ \frac{\partial f_2}{\partial u} \end{bmatrix}, C = \begin{bmatrix} \frac{\partial g}{\partial x_1} & \frac{\partial g}{\partial x_2} \end{bmatrix}$$

Stability

Lyapunov asymptotic stability \iff BIBO stable
 Controllable Observable

State-Space to Transfer Function

$$G(s) = \frac{Y(s)}{U(s)} = C(A-sI)^{-1}B + D$$

$$= \frac{C \cdot \text{Adj}(A-sI) \cdot B}{\det(A-sI)} + D$$

$$= \frac{b_m s^m + \dots + b_1 s + b_0}{s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}$$

Anfangswert: $\lim_{t \rightarrow 0^+} x(t) = \lim_{s \rightarrow \infty} s \cdot X(s)$

Endwert: $\lim_{t \rightarrow \infty} x(t) = \lim_{s \rightarrow 0} s \cdot X(s)$

Reachable Canonical Form

$m < n \rightarrow$

$$\begin{bmatrix} 0 & 1 & 0 & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots \\ -a_0 & -a_1 & -a_2 & \dots & -a_{n-1} & 1 \\ b_0 & b_1 & \dots & b_{n-1} & 0 & 0 \end{bmatrix}$$

$m = n \rightarrow$

$$\begin{bmatrix} 0 & 1 & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ -a_0 & -a_1 & \dots & -a_{n-1} & 1 \\ b_0 - b_n a_0 & b_1 - b_n a_1 & \dots & b_{n-1} - b_n a_{n-1} & 1 \end{bmatrix}$$

Reachability / Observability

$$R = [B \ AB \ \dots \ A^{n-1}B] \quad O = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

$\cdot \det(R) \neq 0 \neq \det(O)$

Important Math

$\cdot \angle \begin{pmatrix} N \\ D \end{pmatrix} = \angle(N) - \angle(D), \angle(a+b)^n = n \angle(a+b)$

$\cdot \angle(z) = \tan^{-1} \left(\frac{\text{Im}}{\text{Re}} \right), \text{Adj}(A) = \begin{bmatrix} d & -b \\ -c & a \end{bmatrix}$

$$\tilde{A}_{\text{reach}} = \begin{bmatrix} \tilde{A}_{r0} & \tilde{A}_{r2} \\ 0 & \tilde{A}_{r0} \end{bmatrix}, \tilde{A}_{\text{obs}} = \begin{bmatrix} \tilde{A}_{o0} & \tilde{A}_{o2} \\ 0 & \tilde{A}_{o0} \end{bmatrix}$$

$$\tilde{B}_{\text{reach}} = [\tilde{B}_1 \ \tilde{B}_2]^T, C_{\text{obs}} = [\tilde{C}_2 \ \tilde{C}_4]$$

⑦ $P_{\text{reach}}(s) \stackrel{!}{=} \det[(\tilde{A}_{\text{reach}} - \tilde{B}_{\text{reach}} K_{\text{reach}}) - sI]$
 $\implies K = \tilde{K}T$

⑧ $P_{\text{obs}}(s) \stackrel{!}{=} \det[(\tilde{A}_{\text{obs}} - \tilde{L}_{\text{obs}} C_{\text{obs}}) - sI]$
 $\implies L = T^{-1} \tilde{L}$

Discrete-time Control

Block diagram: $\text{r}(k) \rightarrow \text{MF} \rightarrow \text{ADC} \rightarrow \text{MP} \rightarrow \text{DAC} \rightarrow \text{PW}$

• Exakt: $s = \frac{1}{T_s} \ln(z), z = e^{sT_s}$

• Euler f: $s = \frac{z-1}{T_s}, z = sT_s + 1$

• Euler b: $s = \frac{z-1}{zT_s}, z = \frac{1}{1-sT_s}$

• Tustin: $s = \frac{z-1}{T_s} \frac{z+1}{z}, z = \frac{1+sT_s}{1-sT_s}$

Sampling Theorem

• No Aliasing: $T_s < \frac{1}{2f_m}, f = \frac{\omega}{2\pi}$

• Theory: $f_s > 2f_{\text{max}}, T_s < \frac{1}{2f_{\text{max}}}$

• Practice: $f_s > 10f_{\text{max}}, T_s < \frac{1}{10f_{\text{max}}}$

Z-Transform

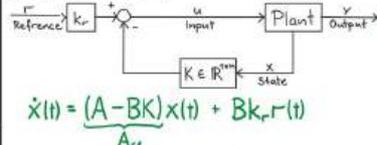
$\cdot Z\{x[k]\} = X(z) = \sum_{k=-\infty}^{\infty} x[k]z^{-k}$

$\cdot Z\{a_1 x_1[k] + a_2 x_2[k]\} = a_1 X_1(z) + a_2 X_2(z)$

$\cdot Z\{x[k-b]\} = X(z)z^{-b}$

$\cdot ZX(z) = Z\{x[k+1]\}$

State Feedback



$$\dot{x}(t) = \frac{(A-BK)x(t) + Bk_r r(t)}{A_{cc}}$$

Reference Tracking

$$k_r = [-C(A-BK)^{-1}B]^{-1} = \frac{a_0 + k_0}{b_0}$$

Achermann Formula (Regulator)

$$K = [0 \ 0 \ \dots \ 1] R^* p_{cc}^*(A) = [k_{n-1} \ \dots \ k_0]$$

Poles placement (2. Order System)

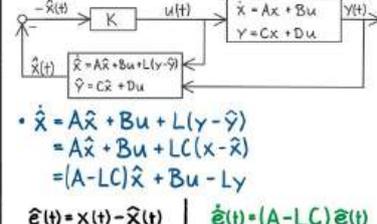
ζ	0.5	1/√2	1
T_r (rise time)	4.8/ω ₀	2.2/ω ₀	2.7/ω ₀
M_p (overshoot)	16%	4%	0%
T_s (settling time)	8.0/ω ₀	5.6/ω ₀	4.0/ω ₀

$$p_{cc}^*(s) \stackrel{!}{=} p_{cc}(s)$$

Higher Order Pole Placement

1. Place dominant pair as usual.
2. Other poles 4x faster than dominant.

State Estimation



$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - \hat{y})$$

$$= A\hat{x} + Bu + LC(x - \hat{x})$$

$$= (A-LC)\hat{x} + Bu + Ly$$

$$\hat{e}(t) = x(t) - \hat{x}(t) \quad \dot{\hat{e}}(t) = -(A-LC)\hat{e}(t)$$

Achermann Formula (Observer)

$$L = p_{cc}^*(A)O^{-1} [0 \ 0 \ \dots \ 1]^T$$

MIMO State-Space

$$\dot{x} = A \cdot x + B \cdot u$$

$$y = C \cdot x + D \cdot u$$

MIMO Transfer-Function

$$P(s) = C(A-sI)^{-1}B$$

$$\begin{bmatrix} Y_1 \\ \vdots \\ Y_r \end{bmatrix} = \begin{bmatrix} P_{1,1}(s) & \dots & P_{1,m}(s) \\ \vdots & \ddots & \vdots \\ P_{r,1}(s) & \dots & P_{r,m}(s) \end{bmatrix} \cdot \begin{bmatrix} U_1 \\ \vdots \\ U_m \end{bmatrix}$$

MIMO Poles/Zeros

Ex: $P(s) = \begin{bmatrix} a & b & c \\ d & e & f \end{bmatrix}$

1. order minors: a, b, c, d, e, f

2. order minors: $\det \begin{bmatrix} a & b \\ c & d \end{bmatrix}, \det \begin{bmatrix} b & c \\ e & f \end{bmatrix}, \det \begin{bmatrix} a & c \\ d & f \end{bmatrix}$

Poles: least common denom. of all minors!

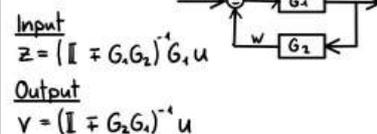
Zeros: greatest common factor of x!

\rightarrow max order minor = $\frac{x}{x}$

• A MIMO-System can have a Pole & a zero at the same Frequency without a Pole-zero cancellation!

• Only possible if there also in the same direction!

MIMO-Interconnection



Design Guidelines for Observer

- Make Observer 10x faster than Controller
- ↑ Observer gain ~ ↑ Measurement noise
- fast Observer ~ large error in transient

Separation Principle

$$\tilde{x} = \begin{bmatrix} x \\ e \end{bmatrix}, \dot{\tilde{x}} = \begin{bmatrix} \dot{x} \\ \dot{e} \end{bmatrix} = \begin{bmatrix} A-BK & BK \\ 0 & A-LC \end{bmatrix} \tilde{x}$$

Control & Estimation do not interact and can be designed independently.

$$(A-BK) \cdot 10 = (A-LC)$$

Popov-Belevitch-Hautus (PBH) Test

- Controllability / Stabilizability:
- $\text{rank}[\lambda I - A \ B] = n, \forall \lambda \in \mathbb{C}$
 - $\text{rank}[\lambda I - A \ B] = n, \forall \lambda \in \mathbb{C}^+$
- Observability / Detectability:
- $\text{rank} \begin{bmatrix} \lambda I - A \\ C \end{bmatrix} = n, \forall \lambda \in \mathbb{C}$
 - $\text{rank} \begin{bmatrix} \lambda I - A \\ C \end{bmatrix} = n, \forall \lambda \in \mathbb{C}^+$

Reachability Decomposition

$\text{rank}(R) = r < n, Z = \begin{pmatrix} z_1 \\ z_2 \end{pmatrix} = TX$

- reachable: $z_1 \in \mathbb{R}^r$ • not: $z_2 \in \mathbb{R}^{n-r}$

$$T^{-1} = \begin{bmatrix} v_1, \dots, v_r & | & v_{r+1}, \dots, v_n \\ \text{Basis of } \mathbb{R} & | & \text{completion} \end{bmatrix}$$

$\rightarrow v_1, \dots, v_r$: linear independent Columns of R

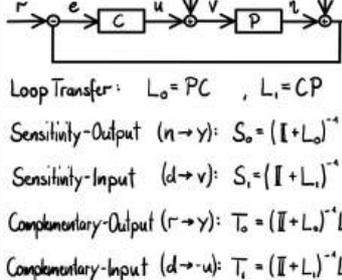
$$\dot{z}_1 = \tilde{A}_{11} z_1 + \tilde{A}_{12} z_2 + \tilde{B}_1 u$$

$$\dot{z}_2 = \tilde{A}_{22} z_2$$

$$y = \tilde{C}_1 z_1 + \tilde{C}_2 z_2 + Du$$

• System $(\tilde{A}_{11}, \tilde{B}_1, \tilde{C}_1, D)$ is reachable

Sensitivity Function



Norms

$\cdot \|x\|_p = \left(\sum |x_i|^p \right)^{1/p}$

$\cdot \|x\|_\infty = \max |x_i|$

$\cdot \|A\|_\infty = \max_i |a_{ij}|$

$\cdot \|A\|_F = \sqrt{\sum_{ij} |a_{ij}|^2} = \sqrt{\text{tr}(G^*G)}$
 L_2 Sum of diag. Elements

Induced Norm:

$\cdot \|A\|_{1,2} = \sqrt{\lambda_{\text{max}}(A^*A)} = \sigma(A)$

Signal Norms:

$e(t) = [e_1(t), \dots, e_n(t)]^T$

$\cdot \|e(t)\|_p = \left(\int_{-\infty}^{\infty} \sum |e_i(t)|^p dt \right)^{1/p}$

$\cdot \|e(t)\|_\infty = \sup(\max(e_i(t)))$
 \rightarrow The supremum is the least upper bound

Singular Value Decomposition (SVD)

$$A = U \Sigma V^*$$

- $A \in \mathbb{C}^{n \times m}, U \in \mathbb{C}^{n \times n}, V \in \mathbb{C}^{m \times m}, \Sigma \in \mathbb{R}^{n \times m}$
- ① Compute $A^*A \in \mathbb{R}^{m \times m}$, symmetric!
- ② Find EW λ_i & EV v_i
- ③ Sort: $\lambda_1 > \lambda_2 > \dots > \lambda_m \geq 0$
 • v_1, v_2, \dots, v_m

Observability Decomposition

$\text{rank}(O) = r < n, Z = \begin{pmatrix} z_1 \\ z_2 \end{pmatrix} = TX$

- observable: $z_1 \in \mathbb{R}^r$ • not: $z_2 \in \mathbb{R}^{n-r}$

$$T^{-1} = \begin{bmatrix} v_1, \dots, v_r & | & v_{r+1}, \dots, v_n \\ \text{completion} & | & \text{Basis of } \ker(O) \end{bmatrix}, T = \begin{bmatrix} u_1 \\ \vdots \\ u_r \\ \vdots \\ u_{n-r} \end{bmatrix}$$

$\rightarrow u_1, \dots, u_r$: linear independent Rows of O

$$\dot{z}_1 = \tilde{A}_{11} z_1 + \tilde{B}_1 u$$

$$\dot{z}_2 = \tilde{A}_{22} z_2 + \tilde{A}_{21} z_1 + \tilde{B}_2 u$$

$$y = \tilde{C}_1 z_1 + \tilde{C}_2 z_2 + Du$$

• System $(\tilde{A}_{11}, \tilde{B}_1, \tilde{C}_1, D)$ is observable

Kalman Decomposition

• System $(A, B, C) \quad Z = \begin{pmatrix} z_1 \\ z_2 \\ z_3 \\ z_4 \end{pmatrix} = TX$

- ① $\text{Im}(R) = \{R_1, R_2\}$ & $\ker(O) = \{O_1, O_2\}$
- ② $H = [\text{Im}(R) | \ker(O)] = [R_1 \ R_2 \ O_1 \ O_2]$
- ③ $\ker(H) = \begin{pmatrix} a \\ 0 \\ a \end{pmatrix}$
- ④ Calculate $X_{r0}, X_{ro}, X_{r\bar{0}}, X_{r0}$:

- $X_{r\bar{0}} = \text{span}\{aR_1 + bR_2\} = \text{span}\{cO_1, dO_2\}$
- $X_{ro}: X_{r0} \oplus X_{ro} = \text{Im}(R)$
- $X_{r\bar{0}}: X_{r0} \oplus X_{r\bar{0}} = \ker(O)$
- $X_{r0}: X_{r0} \oplus X_{ro} \oplus X_{r\bar{0}} \oplus X_{r0} = \mathbb{R}^n$

⑤ $T^{-1} = [X_{r0} | X_{ro} | X_{r\bar{0}} | X_{r0}]$, $T = \dots$

⑥ $\tilde{A} = TAT^{-1}, \tilde{B} = TB, \tilde{C} = CT^{-1}$

$$\tilde{A} = \begin{bmatrix} \tilde{A}_{r0} & \tilde{A}_{r1} & \tilde{A}_{r2} & \tilde{A}_{r3} \\ & \tilde{A}_{r0} & & \\ & & \tilde{A}_{r0} & \tilde{A}_{r1} \\ & & & \tilde{A}_{r0} \end{bmatrix} \quad \tilde{B} = \begin{bmatrix} \tilde{B}_1 \\ \tilde{B}_2 \end{bmatrix}$$

$$\tilde{C} = \begin{bmatrix} \tilde{C}_1 & \tilde{C}_2 \end{bmatrix}$$

continued

④ $Y = [v_1 \ v_2 \ \dots \ v_m] \in \mathbb{C}^{m \times m}$ (normalized?)

⑤ $\Sigma = \begin{bmatrix} \sigma_1 & & & 0 \\ & \sigma_2 & & 0 \\ & & \ddots & \\ 0 & & & \sigma_p \\ & & & & 0 \end{bmatrix} \in \mathbb{R}^{m \times m}, \sigma_i = \sqrt{\lambda_i}$
 \rightarrow same Dim as A?

? $\sigma_1 > \sigma_2 > \dots > \sigma_p > 0, p = \min\{m, n\}$

⑥ $u_i = \frac{1}{\sigma_i} A^* v_i, i = 1, \dots, r, \sigma_i \neq 0$

⑦ Form orthonormal Basis of $\mathbb{C}^{n \times 1}$:

If $r < l$: $\{u_1, u_2, \dots, u_r, u_{r+1}, \dots, u_l\}$
Gram-Schmid

Ex: $\hat{u}_3 = e_3 - (u_1 \cdot e_3)u_1 - (u_2 \cdot e_3)u_2, u_3 = \frac{\hat{u}_3}{\|\hat{u}_3\|}$

⑧ $U = [u_1 \ u_2 \ \dots \ u_l] \in \mathbb{C}^{n \times l}$

• $V^* = \begin{bmatrix} \text{---} \\ \text{---} \\ \vdots \\ \text{---} \end{bmatrix}$ Input Directions (orthogonal!)

• $U = \begin{bmatrix} | & | & \dots & | \\ \text{---} & \text{---} & \dots & \text{---} \\ | & | & \dots & | \end{bmatrix}$ Output Directions (orthogonal!)

SVD Representation

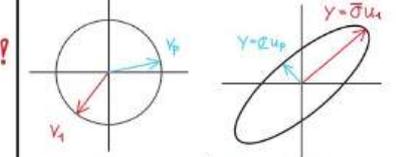
$\sigma_i = \frac{\|Av_i\|}{\|u_i\|}$

$v \rightarrow G \rightarrow Y = Gv$

• Input $\|u_i\| = 1$ • Output:

$v_1 = v_1$ (strong input) $Y = \sigma_1 u_1$ (strong output)

$v_p = v_p$ (weak input) $Y = \sigma_p u_p$ (weak output)



Zero: $Y = Gv_{\text{zero}} = 0$ | Pole: $Y = Gv_{\text{pole}} = \infty$

Pole and Zero Direction from SVD

Pole: $P(s)|_{s=p_i} \cdot \delta_{p_i}^{in} = \infty \cdot \delta_{p_i}^{out}$

$P(p_i) = \begin{pmatrix} u_1 & u_2 \\ \vdots & \vdots \end{pmatrix} \begin{pmatrix} \sigma_{11} & 0 \\ 0 & \sigma_{22} \end{pmatrix} \begin{pmatrix} v_1 & v_2 \\ \vdots & \vdots \end{pmatrix}^T$

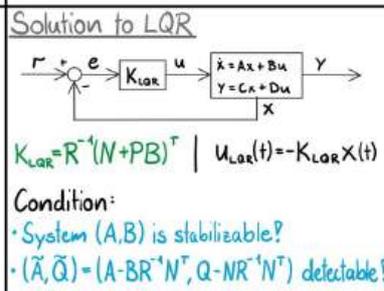
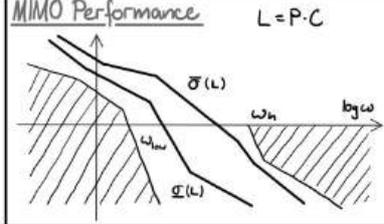
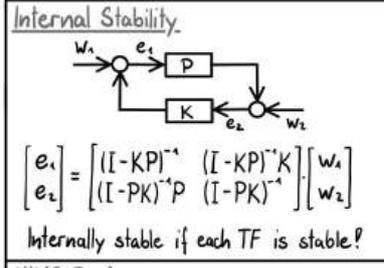
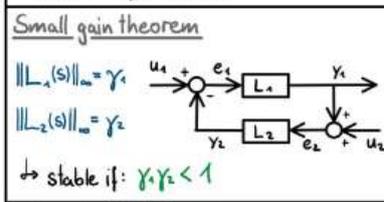
Zero: $P(s)|_{s=z_i} \cdot \delta_{z_i}^{in} = 0 \cdot \delta_{z_i}^{out}$

$P(z_i) = \begin{pmatrix} u_1 & u_2 \\ \vdots & \vdots \end{pmatrix} \begin{pmatrix} \sigma_{11} & 0 \\ 0 & \sigma_{22} \end{pmatrix} \begin{pmatrix} v_1 & v_2 \\ \vdots & \vdots \end{pmatrix}^T$

External Stability

Closed Loop Transferfunction T(s) has Poles in the left hand plane.

↳ BIBO: $\|y\| \leq k \|u\|$



Algebraic Riccati Equations (ARE)

Finding P: P is the **real, symmetric, positive definite** solution of the ARE

$$A^T P + PA - (N+PB)R^{-1}(N^T + B^T P) + Q = 0$$

$$\tilde{A}^T P + P\tilde{A} + P\tilde{R}P + \tilde{Q} = 0$$

$$\tilde{A} = A - BR^{-1}N^T$$

$$\tilde{R} = -BR^{-1}B^T$$

$$\tilde{Q} = Q - NR^{-1}N^T$$

$$P_{2 \times 2} = \begin{bmatrix} \psi_1 & \psi_2 \\ \psi_2 & \psi_3 \end{bmatrix}$$

Hamiltonian

$$H = \begin{bmatrix} \tilde{A} & \tilde{R} \\ -\tilde{Q} & -\tilde{A}^T \end{bmatrix} \quad \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \lambda_1 \dots \lambda_n \\ \lambda_{n+1} \dots \lambda_{2n} \end{bmatrix}$$

$H \in \mathbb{C}^{2n \times 2n}$, $x_1, x_2 \in \mathbb{C}^{n \times 1}$

λ_i are the eigenvectors of H from the **negative** Eigenvalues. (only real λ_i)

⇒ $P = X_2 X_1^{-1}$

Properties

P is **symmetric, real, positive definite**

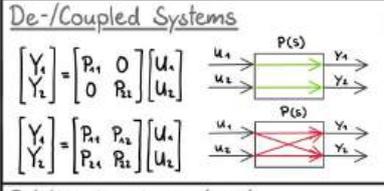
$A - BK_{LQR} = H \rightarrow$ asymptotically stable

Low Frequency

- Output Disturbance Attenuation: $d \rightarrow \eta$
 $\underline{\sigma}(C(j\omega)) \gg 1$
- Input Disturbance Attenuation: $d \rightarrow \nu$
 $\underline{\sigma}(C(j\omega)P(j\omega)) \gg 1$
- Good Tracking: $r \rightarrow e$
 $\underline{\sigma}(P(j\omega)C(j\omega)) \gg 1$

High Frequency

- Output Noise Rejection: $n \rightarrow \eta$
 $\overline{\sigma}(P(j\omega)C(j\omega)) \ll 1$ **Robust Stability**
- Input Noise Rejection: $n \rightarrow \nu$
 $(\underline{\sigma}(P(j\omega)) \gg 1)$ **Can't let go! Controlled!**
- Actuator Saturation: $\overline{\sigma}(C(j\omega)) \ll M$



Relative Gain Array (RGA)

$$RGA(P) = P \times (P^T)^{-1}$$

$P \in \mathbb{C}^{1 \times m}$

$\lambda_{ij} = \frac{\text{gain from } u_j \text{ to } y_i, \text{ all other loops open}}{\text{gain from } u_j \text{ to } y_i, \text{ all other loops closed}}$

If $\lambda_{ij} = 1$: This channel is a SISO System.

If P is upper or lower triangular: $RGA(P) = I$

LQR Properties (N=0)

- infinite positive gain margin (in dB)
- negative gain margin of $20 \log(0.5) = -6 \text{ dB}$
- 60° phase margin (both directions)
- robust stability to additive model uncert.

→ **N: LQR controllers are inherently robust to model uncertainty!**

Linear Quadratic Estimator (LQE)

The Kalman Filter (KF) is the optimal estimator for LTI-systems perturbed by zero mean, Gaussian, process and measurement noises.

→ solve exactly like LQR but with:

$B \rightarrow C^T, A \rightarrow A^T, K \rightarrow L^T$ (if $N=0$)

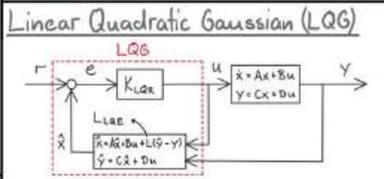
Condition:

- System (A,C) is detectable?
- System (A,Q) is stabilizable?

Solution to LQE (if N=0)

$$AP + PA^T - PC^T R^{-1} C P + Q = 0$$

→ $L = PC^T R^{-1}$



LQG: guarantees stability of CL-system.

- high level approach → macroscopic behaviour
- LQR & LQE provide solid robustness guarantees → **LQG does NOT!**

Tall System ($P \in \mathbb{C}^{1 \times m}, 1 > m$)

Left Moore-Penrose pseudo-inverse:
 $P^+ = (P^* P)^{-1} P^*$, Rank(P) = m

Fat System ($P \in \mathbb{C}^{1 \times m}, 1 < m$)

Right Moore-Penrose pseudo-inverse:
 $P^+ = P^* (P P^*)^{-1}$, Rank(P) = m

General (2x2)-System

$$RGA(P) = \begin{bmatrix} \lambda_{11} & 1-\lambda_{11} \\ 1-\lambda_{22} & \lambda_{22} \end{bmatrix}, \lambda_{ii} = \frac{1}{1 - \frac{P_{12}P_{21}}{P_{11}P_{22}}}$$

RGA interpretation and pairing.

Relevant Frequencies to evaluate RGA:

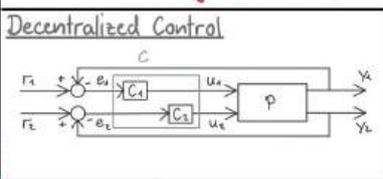
- steady state: $s=0$
- crossover region: $s \in [j\omega_c, j\bar{\omega}_c]$

λ_{ij}	Interpretation	Pairing
1	No interaction from other channels	Yes
0	No effect from j-input to i-output	No
(0,1)	Closing loop increases channel gain	Best if -1
>1	Closing loop decreases channel gain The higher the more interaction	Best if -1
<0	Closed & Open loop gain have opposite sign	No

Diagonal Dominance (RGA)

$$RGA-Mr = \sum_i |RGA(P) - I|$$

↳ low number → diagonally dominant system



Discrete LTI stability

$x[k+1] = r \cdot x[k]$ | $x[k+1] = A_0 x[k] + \dots$

- $r \in (-\infty, -1) \rightarrow$ Div./alt.
- $r \in (-1, 0) \rightarrow$ Con./alt.
- $r \in (0, 1) \rightarrow$ Con./ap.
- $r \in (1, \infty) \rightarrow$ Div./ap.

Continuous A to Discret A0 $s: [v_1, v_2]$

- $e^A = S \cdot \text{diag}(e^{\lambda_1}, e^{\lambda_2}) \cdot S^{-1}$ **eigenvector**
- $\begin{bmatrix} a & b \\ 0 & c \end{bmatrix} = \begin{bmatrix} 1 & \frac{b-a}{a-c} \\ 0 & 1 \end{bmatrix} \begin{bmatrix} a & 0 \\ 0 & c \end{bmatrix} \begin{bmatrix} 1 & \frac{b-c}{c-a} \\ 0 & 1 \end{bmatrix}$

Small gain theorem & Norm calculation

$\|L(j\omega)\|_{\infty} \rightarrow$ Biggest abs. value for $\forall \omega$

Discretization observation

In all cases: $s=0 \rightarrow z=0$: steady state is not affected. (DC-Gain)

Euler forward: (c.t.) stable poles **can map to unstable poles** in (d.t.)

Euler backward: (c.t.) marginally stable poles **can map to stable poles** in (d.t.)

Tustin: (c.t.) stable poles map to (d.t.) stable poles

Matrix Norm

→ if: $\|A \cdot B\| \leq \|A\| \cdot \|B\|$

Decay of Error

$$\dot{e} = (a-b-lc)e \rightarrow \int_{t_0}^{t_1} \frac{de}{e} = \int_{t_0}^{t_1} a-b-lc dt$$

⇒ $\ln\left(\frac{e(t)}{e(t_0)}\right) = (a-b-lc)t$ $\frac{e(t)}{e(t_0)}$: decay of error

Closed Loop

Internally stable if and only if:

- $S_0(s) = (I-P(s)K(s))$ is stable and
- there are no RHP cancellation in $P(s)K(s)$

If $K(s)$ is minimum phase, we cannot conclude anything about internal stability!

Decoupling Control

Intuition: use a "pre-compensator" to diagonalize the plant, then use decentralized control.

① $Y(s) = \frac{P(s)W_1(s)U(s)}{P_2(s)}$

② $C(s) = W_1(s)C_2(s) = W_1(s)C(s)I$

Find $W_1 = \begin{bmatrix} 1 & \delta_{12} \\ \delta_{21} & 1 \end{bmatrix}$: $W_1(s) = P^{-1}(s)$
 $W_1(0) = P^{-1}(0)$
 $W_1(j\omega_c) = P^{-1}(j\omega_c)$

Internal Model Control (IMC)

Q-Parametrization:

- $Q(s) = C(s)(I + P(s)C(s))^{-1}$
- $C(s) = (I - Q(s)P(s))^{-1}Q(s) = Q(s)(I - P(s)Q(s))^{-1}$

Q-internal stability theorem:

- $P(s)$ stable Plant of negative feedback sys. then sys. is internally stable if and only if $Q(s)$ is stable.
- Easy to tune controller, as the sensitivity functions is linearly dependent on $Q(s)$.
- For stable $Q(s)$, stability is guaranteed even if $C(s)$ is unstable.
- Non-minimum phase zeros in the Plant lead to unstable Q-parametrisation.

Linear Quadratic Regulator (LQR)

LQR minimizes J_{LQR} :

$$J_{LQR} = \int_0^{\infty} u(t)^T R u(t) + x(t)^T Q x(t) dt$$

R & Q are diagonal, pos. definite matrices!

Q: cost of a non-zero state.

R: penalizes control effort (input).

Conditional Number

• A measure of "directionality".

Duality

• Duality is a concept that allows to derive conditions on observability based on those for reachability.

Convert Dezibel

$x \text{ dB} = -20 \text{ dB} \cdot \log_{10}(y)$ | $y = 10^{-\frac{x \text{ dB}}{20 \text{ dB}}}$

Singular Value & Input/Output

- $\underline{\sigma}(P(j\omega)) \leq \frac{\|v\|_2}{\|u\|_2} \leq \overline{\sigma}(P(j\omega))$

Transfer Function

$R_2 P_1 (I + R_2 P_1)^{-1}$

$R_2 P_1 (I + R_2 P_1)^{-1}$

$R_1 (I + R_1 P_1)^{-1}$

Hamiltonian

$H = \begin{bmatrix} \tilde{A} & \tilde{R} \\ -\tilde{Q} & -\tilde{A}^T \end{bmatrix}$ $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \lambda_1 \dots \lambda_n \\ \lambda_{n+1} \dots \lambda_{2n} \end{bmatrix}$

$H \in \mathbb{C}^{2n \times 2n}$, $x_1, x_2 \in \mathbb{C}^{n \times 1}$

λ_i are the eigenvectors of H from the **negative** Eigenvalues. (only real λ_i)

⇒ $P = X_2 X_1^{-1}$